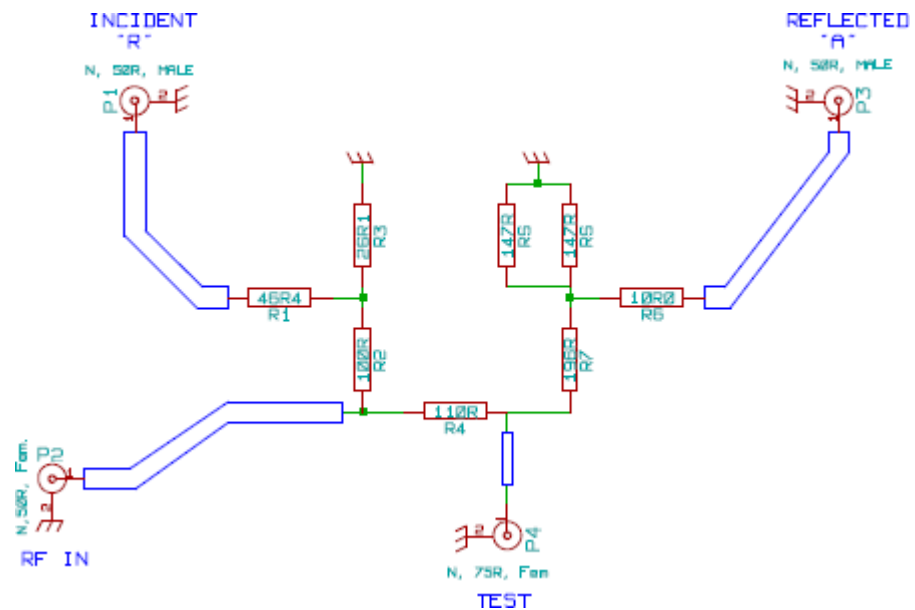


HP87512B (or HP35676B) Sanity Check and Redesign

Source: <https://www.eevblog.com/forum/testgear/cloning-the-hp35676a-reflection-transmission-test-set-for-the-3577ab-vna/msg3126264>

Schematic HP87812B



Parallel resistance function

$$\parallel(R1, R2) := \frac{1}{\frac{1}{R1} + \frac{1}{R2}}$$

Resistor values

$$\begin{aligned} R1 &:= 46.4\Omega & R2 &:= 100\Omega & R3 &:= 26.1\Omega & R4 &:= 110\Omega \\ R5 &:= \frac{147\Omega}{2} = 73.5\Omega & R6 &:= 10\Omega & R7 &:= 196\Omega \\ R_w &:= 50\Omega & R_t &:= 75\Omega \end{aligned}$$

Sanity check

Ref resistance to GND

$$R_{X1} := R1 + R3 \parallel (R2 + R4 + R5 + R7) = 71.153\Omega$$

In resistance to GND

$$R_{X2} := (R2 + R3) \parallel (R4 + R5 + R7) = 94.65\Omega$$

A resistance to GND

$$R_{X3} := R6 + R5 \parallel (R2 + R3 + R4 + R7) = 72.815\Omega$$

Out resistance to GND

$$R_{X4} := (R2 + R3 + R4) \parallel (R5 + R7) = 125.848\Omega$$

Initial analysis

Resistance at X1, Ref

$$R_{S1} := R1 + \left[R3 \parallel \left[R2 + \left[R_w \parallel \left[R4 + \left[R_t \parallel \left[R7 + \left[R5 \parallel (R6 + R_w) \right] \right] \right] \right] \right] \right] \right] = 68.36\Omega$$

Resistance at X2, In

$$R_{S2} := \left[R2 + \left(R1 + R_w \right) \parallel R3 \right] \parallel \left[R4 + \left[R_t \parallel \left[R7 + \left[R5 \parallel (R6 + R_w) \right] \right] \right] \right] = 69.92\Omega$$

Resistance at X3, A

$$R_{S3} := R6 + \left[R5 \parallel \left[R7 + \left[R_t \parallel \left[R4 + \left[R_w \parallel \left[R2 + \left[R3 \parallel (R1 + R_w) \right] \right] \right] \right] \right] \right] \right] = 66.56\Omega$$

Resistance at X4, Out

$$R_{S4} := \left[R7 + \left[R5 \parallel (R6 + R_w) \right] \right] \parallel \left[R4 + \left[R_w \parallel \left[(R1 + R_w) \parallel R3 \right] + R2 \right] \right] = 88.92\Omega$$

T attenuator resistance at X2

$$R_{X2G} := (R_w + R1) \parallel R3 + R2 = 120.54\Omega$$

T attenuator resistance at X4

$$R_{X4G} := (R_w + R6) \parallel R5 + R7 = 229.03\Omega$$

Insertion loss R_t terminated $A_{X24} := 20\text{dB} \log \left(\frac{2}{\frac{R_w}{R_{S2}} + 1} \cdot \frac{1}{\frac{R4}{R_{X4G} \parallel R_t} + 1} \right) = -8.05 \cdot \text{dB}$

Insertion loss X4 open $A_{X24o} := 20\text{dB} \log \left(\frac{2}{\frac{R_w}{R_{S2}} + 1} \cdot \frac{1}{\frac{R4}{R_{X4G}} + 1} \right) = -2.07 \cdot \text{dB}$

Note: The insertion loss X2 to X4 calculated above is based on the voltage ratio. Due to the fact that the nominal X4 port load is $R_t = 75 \cdot \Omega$, while the X2 input power is based on $R_w = 50 \cdot \Omega$, the voltage ratio must be adjusted by k_t to obtain the actual insertion loss as the power ratio X2 to X4 in [dB].

Power at R_w and R_t $P_w = \frac{U_L^2}{R_w}$ $P_t = \frac{U_L^2}{R_t}$

Correction factor $R_w - R_t$ $k_t = 10\text{dB} \log \left(\frac{P_t}{P_w} \right) := 10\text{dB} \log \left(\frac{R_w}{R_t} \right) = -1.76 \cdot \text{dB}$

Power loss R_t terminated $A_{pX24} := A_{X24} + k_t = -9.814 \cdot \text{dB}$

T attenuator X2 - X1 $A_{X21} := 20\text{dB} \log \left[\frac{1}{\frac{R2}{(R1 + R_w) \parallel R3} + 1} \cdot \frac{1}{\frac{R1}{R_w} + 1} \right] = -21.07 \cdot \text{dB}$

T attenuator X4 - X3 $A_{X43} := 20\text{dB} \log \left[\frac{1}{\frac{R7}{(R6 + R_w) \parallel R5} + 1} \cdot \frac{1}{\frac{R6}{R_w} + 1} \right] = -18.4 \cdot \text{dB}$

Redesign

To calculate the 7 resistance values the following 7 conditions shall be met:

1. the resistance R_{S1} at X1 shall be R_w when X2, X3 and X4 are loaded with R_w
2. the resistance R_{S2} at X2 shall be R_w when X1, X3 and X4 are loaded with R_w
3. the resistance R_{S3} at X3 shall be R_w when X1, X2 and X4 are loaded with R_w
4. the resistance R_{S4} at X4 shall be R_w when X1, X2 and X3 are loaded with R_t
5. the insertion loss A_{X24} of the signal path from X2 to X4 shall be $10\text{dB}-k_t = 8.2\text{dB}$ when X1 and X3 are loaded with R_w
6. the attenuation A_{X21} of the T attenuator from X2 to X1 shall be 21dB when X3 and X4 are loaded with R_w
7. the attenuation A_{X43} of the T attenuator from X4 to X3 shall be 18dB when X1 and X2 are loaded with R_w and R_t , respectively

Given

Condition 1: $R_{X1} = R_w$

$$R_w = R1 + \frac{1}{\frac{1}{R3} + \frac{1}{R2 + \frac{1}{\frac{1}{R_w} + \frac{1}{R4 + \frac{1}{\frac{1}{R_t} + \frac{1}{R7 + \frac{1}{\frac{1}{R5} + \frac{1}{R6 + R_w}}}}}}}}$$

Condition 2: $R_{X2} = R_w$

$$R_w = \frac{1}{\frac{1}{R2 + \frac{1}{\frac{1}{R1 + R_w} + \frac{1}{R3}}} + \frac{1}{R4 + \frac{1}{\frac{1}{R_t} + \frac{1}{R7 + \frac{1}{\frac{1}{R5} + \frac{1}{R6 + R_w}}}}}}$$

Condition 3: $R_{X3} = R_w$

$$R_w = R6 + \frac{1}{\frac{1}{R5} + \frac{1}{R7 + \frac{1}{\frac{1}{R_t} + \frac{1}{R4 + \frac{1}{\frac{1}{R_w} + \frac{1}{R2 + \frac{1}{\frac{1}{R3} + \frac{1}{R1 + R_w}}}}}}}}$$

Condition 4: $R_{X4} = R_t$

$$R_t = \frac{1}{\frac{1}{R7 + \frac{1}{\frac{1}{R5} + \frac{1}{R6 + R_w}}} + \frac{1}{R4 + \frac{1}{\frac{1}{R_w} + \frac{1}{R2 + \frac{1}{\frac{1}{R1 + R_w} + \frac{1}{R3}}}}}}$$

Condition 5: $A_{x24} = 8.2\text{dB}$

$$10^{\frac{-8.2}{20}} = \frac{2}{R_w \left(\frac{1}{R2 + \frac{1}{\frac{1}{R1 + R_w} + \frac{1}{R3}}} + \frac{1}{R4 + \frac{1}{\frac{1}{R_t} + \frac{1}{R7 + \frac{1}{\frac{1}{R5} + \frac{1}{R6 + R_w}}}}} \right) + 1} \cdot \frac{1}{R4 \left(\frac{1}{\frac{1}{R_w + R6} + \frac{1}{R5}} + R7 + \frac{1}{R_t} \right) + 1}$$

Condition 6: $A_{x21} = 21\text{dB}$

$$10^{\frac{-21}{20}} = \frac{1}{R2 \left(\frac{1}{R1 + R_w} + \frac{1}{R3} \right) + 1} \frac{1}{\frac{R1}{R_w} + 1}$$

Condition 7: $A_{x43} = 18\text{dB}$

$$10^{\frac{-18}{20}} = \frac{1}{R7 \left(\frac{1}{R6 + R_w} + \frac{1}{R5} \right) + 1} \frac{1}{\frac{R6}{R_w} + 1}$$

solved for resistor values

$$R_v := \text{Find}(R1, R2, R3, R4, R5, R6, R7) = \begin{pmatrix} 37.69 \\ 65.15 \\ 14 \\ 86.66 \\ 59.01 \\ 3.18 \\ 180.92 \end{pmatrix} \Omega$$

E96 factor

$$e_{96} := 10^{\frac{1}{96}} = 1.024$$

Function to convert to E96 values

$$R_N(R) := \text{round} \left(100 e_{96}^{\left(\frac{\text{round} \left(\frac{\ln \left(\frac{R}{10\Omega} \right)}{\ln(e_{96})} \right)}{\ln(e_{96})} \right)} \right) 0.1\Omega$$

New resistors R1, R2

$$R1 := R_N(R_{v0}) = 37.4 \Omega$$

$$R2 := R_N(R_{v1}) = 64.9 \Omega$$

New resistors R3, R4

$$R3 := R_N(R_{v2}) = 14 \Omega$$

$$R4 := R_N(R_{v3}) = 86.6 \Omega$$

New resistors R5, R6

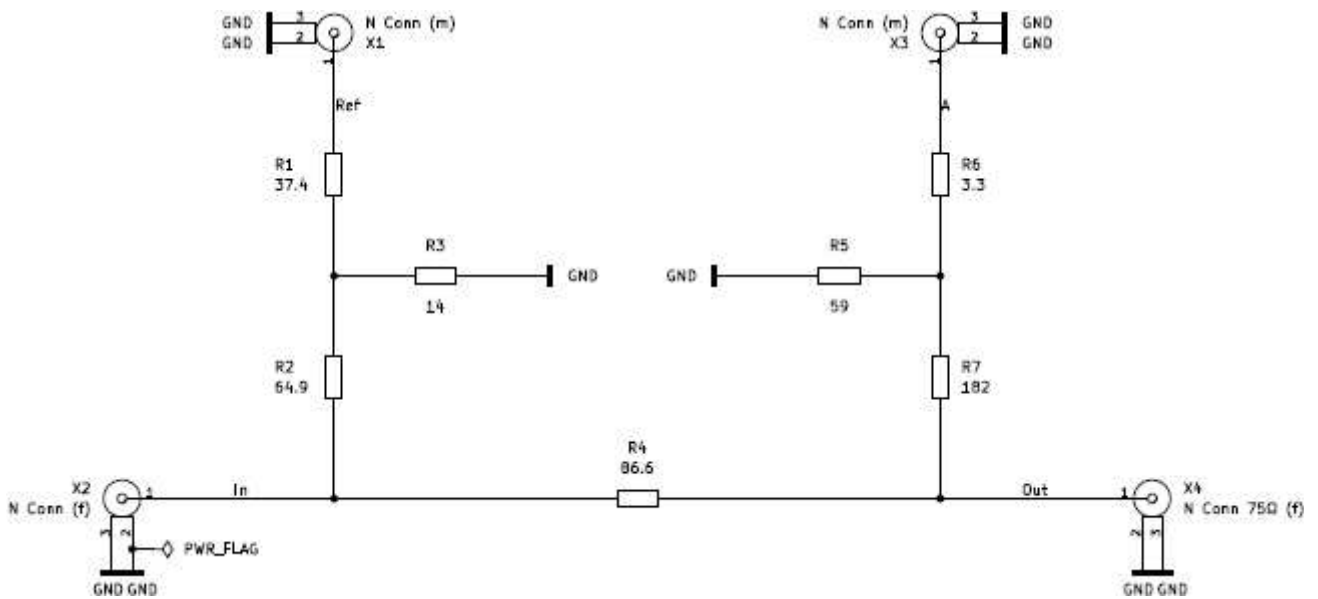
$$R5 := R_N(R_{v4}) = 59 \Omega$$

$$R6 := R_N(R_{v5}) = 3.3 \Omega$$

New resistor R7

$$R7 := R_N(R_{v6}) = 182 \Omega$$

Analysis with redesigned resistor values



Resistance at X1, Ref

$$R_{S1} := R1 + [R3 \parallel [R2 + [R_w \parallel [R4 + [R_t \parallel [R7 + [R5 \parallel (R6 + R_w)]]]]]] = 49.71 \Omega$$

Resistance at X2, In

$$R_{S2} := [R2 + (R1 + R_w) \parallel R3] \parallel [R4 + [R_t \parallel [R7 + [R5 \parallel (R6 + R_w)]]]] = 49.9 \Omega$$

Resistance at X3, A

$$R_{S3} := R6 + [R5 \parallel [R7 + [R_t \parallel [R4 + [R_w \parallel [R2 + [R3 \parallel (R1 + R_w)]]]]]] = 50.06 \Omega$$

Resistance at X4, Out

$$R_{S4} := [R7 + [R5 \parallel (R6 + R_w)]] \parallel [R4 + [R_w \parallel [(R1 + R_w) \parallel R3] + R2]] = 75.11 \Omega$$

T attenuator resistance at X2

$$R_{X2G} := (R_w + R1) \parallel R3 + R2 = 76.97 \Omega$$

T attenuator resistance at X4

$$R_{X4G} := (R_w + R6) \parallel R5 + R7 = 210.08 \Omega$$

Insertion loss R_t terminated

$$A_{X24} := 20\text{dB} \log \left(\frac{2}{\frac{R_w}{R_{S2}} + 1} \cdot \frac{1}{\frac{R4}{R_{X4G} \parallel R_t} + 1} \right) = -8.2 \cdot \text{dB}$$

Insertion loss X2 - X4 open

$$A_{X24o} := 20\text{dB} \log \left(\frac{2}{\frac{R_w}{R_{S2}} + 1} \cdot \frac{1}{\frac{R4}{R_{X4G}} + 1} \right) = -3.01 \cdot \text{dB}$$

Power loss R_t terminated

$$A_{pX24} := A_{X24} + k_t = -9.96 \cdot \text{dB}$$

T attenuator X2 - X1

$$A_{X21} := 20\text{dB} \log \left[\frac{1}{\frac{R2}{(R1 + R_w) \parallel R3} + 1} \cdot \frac{1}{\frac{R1}{R_w} + 1} \right] = -20.94 \cdot \text{dB}$$

T attenuator X4 - X3

$$A_{X43} := 20\text{dB} \log \left[\frac{1}{\frac{R7}{(R6 + R_w) \parallel R5} + 1} \cdot \frac{1}{\frac{R6}{R_w} + 1} \right] = -18.05 \cdot \text{dB}$$